

Nyquist Frequency in Sequentially Sampled Data

Faghih, Nezameddin and Faghih, Ali

Shiraz University, University of Maryland

2008

Online at https://mpra.ub.uni-muenchen.de/14311/ MPRA Paper No. 14311, posted 27 Mar 2009 03:22 UTC

Nyquist Frequency in Sequentially Sampled Data

Nezameddin Faghih* and Ali Faghih**

ABSTRACT

This paper studies the sequential sampling scheme as a solution to the problem of aliasing, where the sampling interval is restricted to a minimum allowable value ΔT . In sequential sampling, the signal is sampled at intervals of ΔT , $\Delta T + \Delta \tau$, $\Delta T + 2\Delta \tau$, $\Delta T + 3\Delta \tau$, ...; where $\Delta \tau < \Delta T$ and $\Delta \tau$ may be selected as desirable. Sequential sampling is, however, analyzed and it is proved that when the ratio $\Delta T/\Delta \tau$ is an integral number, the associated spectral estimates give a Nyquist frequency $\frac{1}{2\Delta \tau}$. This sampling scheme can, therefore, be employed to yield a required cut- off frequency.

* Shiraz University (<u>faghihnezam@ut.ac.ir</u>)

** University of Maryland, College Park

INTRODUCTION

Some data acquisition systems have a minimum allowable sampling interval and do not provide a desired sampling period less than a minimum allowable value. This may be due to some restrictions set by the measuring instrument that has to be used [1-7].

Let the minimum allowable sampling time be ΔT ; if the uniform sampling scheme is employed then, the Nyquist or cut-off frequency is known [8] to be given as:

$$f_{c} = \frac{1}{2\Delta T}$$
(1)

This would mean that if frequencies higher than f_c are present, aliasing will occur. Otherwise, the signal would have to be filtered so that only frequencies below f_c are passed and, therefore, the spectral analysis will be restricted [8].

The sequential sampling scheme can, however, be employed to obtain an autocorrelation function with estimates $\Delta \tau$ apart, where $\Delta \tau < \Delta T$, with the exception of coefficients lying inside the range R(0) \rightarrow R(ΔT). In this sampling scheme, the signal would be sampled at intervals of:

 ΔT , ΔT + $\Delta \tau$, ΔT + $2\Delta \tau$, ΔT + $3\Delta \tau$, ...

From the sampled signal, an autocorrelation function can be obtained with the coefficients:

 $R(0), R(\Delta T), R(\Delta T + \Delta \tau), R(\Delta T + 2\Delta \tau), \dots$

While ΔT is restricted, the value of $\Delta \tau$ may be chosen as desirable. It will be proved, in this paper, that the sequential sampling can give an increased cut-off frequency as:

$$f_{cs} = \frac{1}{2\Delta\tau}$$
(2)

The sequential sampling can, therefore, be employed to overcome aliasing and the restrictions of spectral analysis, by selecting a sufficiently small value for $\Delta \tau$.

THE CUT OFF FREQUENCY IN THE SEQUENTIAL SAMPLING

The cut- off frequency provided by the sequential sampling scheme is considered in this section. The analysis employs the impulse representation of a continuous signal as an approach to discretization [9-14].

In the sequential sampling, the signal is sampled at intervals of:

 ΔT , ΔT + $\Delta \tau$, ΔT +2 $\Delta \tau$, ΔT +3 $\Delta \tau$, ...

The sampling instants are, therefore, given by:

 $t_i = 0, \quad \Delta T, 2\Delta T + \Delta \tau, 3\Delta T + 3\Delta \tau, 4\Delta T + 6\Delta \tau, \dots$ (3) This can be written as:

$$t_i = i\Delta T + [\sum_{r=0}^{i} r - i]\Delta \tau, \quad i = 0, 1, 2, 3, ...$$
 (4)

Since,
$$\sum_{r=0}^{i} r = \frac{i}{2} (i + 1)$$
, then equation (4) gives:

$$t_{i} = i\Delta T + \frac{i}{2}(i-1)\Delta\tau$$
(5)

When a continuous signal x(t) is sampled, the sample values $x(t_i)$ are acquired. A discrete autocorrelation function, with coefficients $R(\tau_j)$, may be obtained from the discrete signal, by contributions of the products $x(t_i)x(t_{i+i})$. Equation (5) can be used to give the time delay τ_i as:

$$\tau_{j} = t_{i+j} - t_{i} = \Delta T + \left[\frac{j}{2}(j-1) + ij + (j-1)\mu\right] \Delta \tau$$
(6)

where μ is a constant given by:

$$\mu = \Delta T / \Delta \tau \tag{7}$$

It is seen from equation (6) that for j=0, the time delay is zero and for j=1, the time delay is $\Delta T+i\Delta \tau$ (where i=0, 1, 2,3, ...). An autocorrelation function is, therefore, obtainable at discrete values of the time delay given as:

$$\tau_n = 0, \Delta T + n \Delta \tau n = 0, 1, 2, 3, ...$$
 (8)

If the ratio μ is an integral number, then higher values of j would also provide more contributions to the autocorrelation estimates at the above time delays τ_n . This is because j(j-1)/2 is always even, and any value of j would hence add a multiple of $\Delta \tau$ to ΔT .

The discrete autocorrelation function may be represented as:

$$\mathbf{R}^{*}(\tau) = \Delta \tau. \mathbf{R}(\tau) \delta_{\mathbf{b}}(\tau)$$
(9)

where $R(\tau)$ is the continuous autocorrelation function and $\delta_b(\tau)$ is the following form of the delta comb:

$$\delta_{\mathbf{b}}(\tau) = \delta(\tau) + \delta(\tau - \Delta T) + \delta(\tau - \Delta T - \Delta \tau) + \delta(\tau - \Delta T - 2\Delta \tau) + \mathbf{L}$$
(10)

It is established [9-10] that the Fourier transform of equation (10) can be written as:

$$\Delta_{b}(\omega) = 1 + e^{-j\omega\Delta T} \sum_{0}^{\infty} e^{-j\omega n\Delta \tau}$$
(11)

which by manipulation [9-10] can be re-written as:

$$\Delta_{b}(\omega) = \frac{1 - e^{-j\omega\Delta\tau} + e^{-j\omega\mu\Delta\tau}}{1 - e^{-j\omega\Delta\tau}}$$
(12)

where substitution has also been made for ΔT from equation (7).

The Fourier transformation of $R^*(\tau)$ gives the spectral density $S^*(\omega)$ corresponding to the sampled signal and that of $R(\tau)$ would yield the spectral density $S(\omega)$ of the original continuous signal. The approach adopted for the Fourier transformation of equation (9) is based on the convolution and residue theorems [9]. By evaluating the residue terms [9] and using the convolution property [9], for substitution into equation (9), the Fourier transform of this equation ca be obtained as:

$$S^{*}(\omega) = \sum_{-\infty}^{\infty} e^{j2\pi n\mu} S(\omega + 2n\omega_{cs}), \quad \omega_{cs} = \pi_{/\Delta\tau}$$
(13)

However, if the ratio $\mu = (\Delta T / \Delta \tau)$ is an integral number then,

 $e^{j2\pi n\mu} = 1$

noting that n is also an integer. Substituting this into equation (13) gives:

$$S^{*}(\omega) = \sum_{-\infty}^{\infty} S(\omega + 2n\omega_{cs}), \quad \omega_{cs} = \pi_{/\Delta\tau}$$
(14)

Now, consider the periodicity of $S^*(\omega)$; this can also be examined by applying the corresponding methods [9-14]. Using equations (9), (10), (11) and the rules established for discrete Fourier transformation [9-10], it can be written:

$$\Delta \tau [R(0) + e^{-j\omega\Delta T} \sum_{0}^{\infty} R(\Delta T + n\Delta \tau) e^{-j\omega n\Delta \tau}] = \Delta \tau [R(0) + e^{-j\omega\mu\Delta \tau} \sum_{0}^{\infty} R(\Delta T + n\Delta \tau) e^{-j\omega n\Delta \tau}] (15)$$

and then for an integer m:

$$\Delta \tau [R(0) + e^{-j(\omega + 2m\omega_{cs})\mu\Delta\tau} \sum_{0}^{\infty} R(\Delta T + n\Delta\tau) e^{-j(\omega + 2m\omega_{cs})n\Delta\tau}] = \Delta \tau [R(0) + e^{-j\omega\mu\Delta\tau} e^{-j2m\omega_{cs}\mu\Delta\tau} \sum_{0}^{\infty} R(\Delta T + n\Delta\tau) e^{-j\omega n\Delta\tau} . e^{-j2m\omega_{cs}n\Delta\tau}] = \Delta \tau [R(0) + e^{-j\omega\mu\Delta\tau} . e^{-j2m\mu\pi} \sum_{0}^{\infty} R(\Delta T + n\Delta\tau) e^{-j\omega n\Delta\tau} . e^{-j2mn\pi}] = \Delta \tau [R(0) + e^{-j\omega\mu\Delta\tau} . e^{-j2m\mu\pi} \sum_{0}^{\infty} R(\Delta T + n\Delta\tau) e^{-j\omega n\Delta\tau}]$$
(16)

since m and n are integers. If μ is also an integral number, this would reduce to:

$$\Delta \tau [R(0) + e^{-j\omega\mu\Delta\tau} \sum_{0}^{\infty} R(\Delta T + n\Delta\tau) e^{-j\omega n\Delta\tau}]$$

from which it follows that:

$$\mathbf{S}^*(\omega + 2\mathbf{m}\omega_{cs}) = \mathbf{S}^*(\omega) \tag{17}$$

This is the mathematical statement for $S^*(\omega)$ to be periodic with period $2\omega_{cs}$. Otherwise, if μ is not an integral number,

$$\mathbf{S}^{*}(\boldsymbol{\omega} + 2\mathbf{m}\boldsymbol{\omega}_{cs}) \neq \mathbf{S}^{*}(\boldsymbol{\omega})$$
(18)

and the requirement for periodicity is not met.

It is, therefore, seen that when the ratio $\mu(=\Delta T/\Delta \tau)$ is an integral number, the periodic pattern, conforming with the Nyquist theorem,[9-14] is obtained. That is, the sequential sampling gives a cut-off frequency $\omega_{cs} = \pi/\Delta \tau$ or $f_{cs} = \frac{1}{2\Delta \tau}$. On the contrary, when μ is not a whole number, $S^*(\omega)$ is related to the true spectral density by equation (13); it includes a complex term and is not periodic.

CONCLUSIONS

This paper has considered the sequential sampling scheme, as a solution to the problem of aliasing, where the sampling interval is restricted to a minimum allowable value ΔT . In the sequential sampling, the signal is sampled at intervals of ΔT , $\Delta T + \Delta \tau$, $\Delta T + 2\Delta \tau$, $\Delta T + 3\Delta \tau$,...; where $\Delta \tau p \Delta T$ and may be selected as desirable.

The sequential sampling was considered analytically and it was proved that, when the ratio $\Delta T / \Delta \tau$ is an integral number, the corresponding spectral estimates give a cut- off frequency of $\frac{1}{2\Delta\tau}$. On the contrary, when the ratio is not a whole number, the associated spectrum of the sequentially

sampled data was found to comprise a complex term in its relation to the true spectrum and would not be periodic in terms of the cut-off frequency.

REFERENCES

- 1 Wirth, W.D. (1995), "Energy Saving by Coherent Sequential Detection of Radar Signals with Unknown Doppler Shift", IEE Proceedings on Radar, Sonar and Navigation, 142, 145-52.
- 2 Willis, N.P. and Bresler, Y.(1992), "A New Approach to the Time-Sequential Sampling Problem", Proceedings of the IEEE International Conference on Acoustics, Speech and Signal Processing, 3, 277-80.
- 3 Allebach, J.P. (1984), "Design of Antialiasing Patterns for Time-Sequential Sampling of Spatiotemporal Signals", IEEE Transactions on Acoustics, Speech and Signal Processing, 32, 1, 137-44.
- 4 Allebach, J.P. (1981), "Design of Sampling Patterns for Time Sequential Sampling of Spatio- Temporal Signals", Proceedings of Micro-Delcon Delaware Bay Computer Conference, 9-13.
- 5 Aizawa, A.N. and Wah, B.W. (1994), "A Sequential Sampling Procedure for Genetic Algorithms", Computer and Mathematics with Applications, 27, 9-10, 77-82.
- 6 Gaster, M. and Bradbury, L.J.S. (1976), "The Measurement of the Spectra of Highly Turbulent Flows by a Randomly Triggered Pulsed-Wire Anemometer", J. Fluid Mech, 77, 499-509.
- 7 Bradbury, L.J.S. (1978), "Examples of the Use of the Pulsed Wire Anemometer in Highly Turbulent Flow", Proceedings of the Dynamic Flow Conference, Marseille, 489-509.
- 8 Bendat, J.S. and Piersol, A.G. (1986), "Random Data: Analysis and Measurement Procedures", Wiley-Interscience.
- 9 Saucedo, R. and Schiring, E. (1968), "Introduction to Continuous and Digital Control Systems", Macmillan.
- 10 Papoulis, A. (1962), "The Fourier Integral and its Applications", McGraw-Hill.

- 11 Oppenheim, A.V. et al (1983), "Signals and Systems", Prentice- Hall.
- 12 Carlson, A.B. (1986), "Communication Systems", McGraw-Hill.
- 13 Jones, R.H. and Steele, N.C. (1989), "Mathematics in Communication Theory", Ellis Horwood Publishers.
- 14 Steward, E.G. (1989), "Fourier Optics: an Introduction", Ellis Horwood Publishers.